

**FOUNDRY BINDER COMPOSITIONS AND MIXES THAT
CONTAIN A DIVALENT SULFUR COMPOUND**

FIELD OF THE INVENTION

5 This invention relates to foundry binder compositions that contain a divalent sulfur compound, and/or foundry mixes where the aggregate contains a divalent sulfur compound. The foundry binders and foundry mixes are used to make foundry shapes, e.g. molds and cores. The presence of sulfur in the foundry shape facilitates the removal of foundry shapes (particularly internal cores) from the metal casting which is
10 made by pouring molten metal into a casting assembly in which the foundry shapes are arranged. The invention also relates to a method of preparing foundry shapes, the shapes prepared, a method of making a metal casting, and metal castings by this process.

BACKGROUND OF THE INVENTION

15 In the foundry industry, one of the procedures used for making metal parts is "sand casting". In sand casting, disposable molds and cores are fabricated with a mixture of sand and an organic or inorganic binder. The foundry shapes are arranged in casting assembly, which results in a cavity through which molten metal will be poured.
20 After the molten metal is poured into the assembly of molds and cores and cools, the metal part formed by the process is removed from the assembly. The binder is needed so the molds and cores will not disintegrate when they come into contact with the molten metal.

 Two of the prominent fabrication processes used in sand casting are the no-bake
25 and the cold-box processes. In the no-bake process, a liquid curing catalyst is mixed with an aggregate and binder to form a foundry mix before shaping the mixture in a pattern. The foundry mix is shaped by putting it into a pattern and allowing it to cure until it is self-supporting and can be handled. In the cold-box process, a gaseous curing catalyst is passed through a shaped mixture (usually in a corebox) of the aggregate and
30 binder to cure the mixture.

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A binder commonly used in the cold-box fabrication process is a phenolic urethane binder. The phenolic urethane binder is mixed with an aggregate to form a foundry mix. The foundry mix is blown into pattern, typically a corebox, where it is cured by passing a gaseous tertiary amine catalyst through it. The phenolic urethane binder consists of a phenolic resin component and polyisocyanate component. Phenolic urethane binders are widely used in the foundry industry to bond the sand cores used in casting iron and aluminum. An example of a commonly used phenolic-urethane binder used in the cold-box process is disclosed in U.S. Patent 3,409,575.

One of the problems with the using organic binders to form foundry shapes is that they can be too effective in binding the aggregate together. The result is that the foundry shapes are not readily separated from the metal part formed during the casting process. Consequently, time consuming and labor intensive means must be utilized to break down the binder so the metal part can be removed from the casting assembly. This is particularly a problem with internal cores, which are imbedded in the casting assembly and not easily removed.

The phenolic urethane cold-box process can be used to make cores and molds for the casting of ferrous and non-ferrous metal parts. Since iron castings are manufactured at about 1500° C, any phenolic urethane binder used in making foundry shapes, i.e. internal cores, will undergo rapid thermal decomposition at this temperature. Because of this, the internal core can be easily separated from the iron casting. This does not occur when aluminum parts are cast because aluminum castings are manufactured at about 700° C. At this lower temperature, the phenolic urethane binder does not readily decompose when the aluminum is cast, thus making complete removal of an internal core difficult.

Since light alloy casting, such as aluminum casting, is becoming increasingly used in place of iron as a means of reducing the weight of vehicle components such as engine blocks and manifolds, there is a need for developing new methods which facilitate the removal of internal cores. One method of facilitating removal of an internal core from a large aluminum casting (e.g. an engine block) or a complex aluminum casting (e.g. a water pump housing), is by baking the casting in a forced air

oven at a high temperature for five to ten hours until the binder slowly decomposes. This procedure reduces productivity and requires forced air ovens and large amounts of energy. Alternatively, some aluminum castings can be violently shaken until the internal core is released. This procedure is inefficient and also reduces productivity.

5 Alternatives to phenolic-urethane cold-box binder systems can be used for aluminum casting that afford good core removal. For example, furan cold-box resins display excellent core removal characteristics in aluminum casting. However, furan resin binders build a tar like residue on tooling. This requires frequent cleaning, higher tooling costs, and lowers foundry productivity. See Richardson U.S. 3,879,339.

10 It is also known to use additives to improve the core removal characteristics of phenolic binders. For example, Ohashi et al, U.S. 4,600,733, teaches that a "disintegration assistant" composed mainly of calcium hydroxide, calcium carbonate, barium hydroxide and/or barium carbonate will promote heat deterioration of condensation resins such as phenolic shell resins. Another example is described in
15 Japanese Abstract J.P. 60,064,744, which discloses that metal bromides promote the collapsibility phenolic shell resins. S.U. Abstract 1,316,741 discloses the use of a water glass binder in mixture with iron oxide, sulfur, and silica based refractory filler that has improved knockout. The iron oxide is added to breakdown the binder which improves the knockout capability of the mixture.

20

SUMMARY OF THE INVENTION

This invention relates to foundry binder compositions comprising as a mixture:

- 25
- (a) an organic foundry binder having at least one component; and
 - (b) an effective amount of a divalent sulfur compound where said divalent sulfur compound is present in at least one component of the binder.

An effective amount of divalent sulfur compound is an amount sufficient to facilitate removal of a foundry shape from a metal casting, where the foundry shape is made from the organic binder containing the divalent sulfur compound.

5 The invention also relates to foundry binder systems where (a) and (b) are separate components, and foundry mixes that contain a divalent sulfur compound in the foundry aggregate. The invention also relates to a method of preparing a foundry shape, the shapes prepared, a method of making a metal casting, and metal castings prepared by this process.

10 The presence of sulfur in the binder composition and/or the aggregate facilitates the separation of the foundry shapes (cores and molds) from the metal part made by pouring molten metal into the foundry assembly. The effect of the sulfur in the foundry mix is particularly noteworthy when making aluminum parts with a casting assembly having internal cores. The time needed to remove the internal core from the metal part is significantly reduced which reduces cost and increased productivity.

15 These sulfur-containing organic binder compositions and/or foundry mixes are preferred for the cold-box process using phenolic urethane binders. Their advantages are most apparent when used to make internal cores that will be used in a casting assembly to cast aluminum parts.

20 **BEST MODE AND OTHER EMBODIMENTS
OF THE INVENTION**

This invention can be used in any process, which utilizes an organic binder for making foundry shapes. For purposes of describing this invention, a foundry shape is
25 any shape made from a foundry aggregate and organic binder that is used in a molding assembly for casting metal parts. A casting assembly is an arrangement of foundry shapes in a pattern such that a metal casting will be produced when molten metal is poured into the casting assembly and allowed to cool. An internal core is a core that is imbedded in the casting assembly. A foundry mix is a mixture of a foundry binder, and
30 aggregate, and possibly a curing catalyst.

The action of sulfur to promote removal of organically bound cores can be enhanced with catalysts. For instance, nucleophilic, electrophilic, and free radical catalysts are known to cleave S-S bonds and create polysulfides that are more reactive than cyclooctasulfur. "Reactions of Sulfur with Organic Compounds", Voronkov, M.

5 G. et. al., Consultants Bureau of New York, a Division of Plenum Publishing New York, New York (1987, pages 40-45, QD 412.S1R37 ISBN 0-303-10978-6). The action of sulfur can also be enhanced with phosphines, organomagnesium compounds, group IVA organometallic compounds, amines, sulfides, polysulfides, mineral and organic protic acids, Lewis acids such as boron and aluminum compounds, copper,
10 zinc, platinum, activated charcoal, zinc sulfide, fluorides, metal oxides. Free radical generators such as peroxides, persulfates, azo compounds, and the like could also augment the action of sulfur.

The sulfur is added to the foundry aggregate and/or one or more of the components of the organic binder, where the component may be reactive or non
15 reactive. As was mentioned before, one of the preferred organic binders is a phenolic urethane binder cured by an amine catalyst. This binder comprises a phenolic resin component or and organic polyisocyanate component, both of which are reactive components. The divalent sulfur compound can be added to either of these components.

20 The divalent sulfur compound can also be dissolved or dispersed in a liquid or solid medium before it is added to the foundry aggregate or the organic binder. Examples of liquid media that can be used to dissolve the divalent sulfur compound are solvents, e.g. carbon disulfide, petroleum distillate, or a resin such as a phenolic resin. The divalent sulfur compound can also be dispersed in a dry medium such as a foundry
25 additive mixture as disclosed in U.S. Patent 4,735,973 and the like. Although a dispersant may be used in some situations to improve the dispersability of the divalent sulfur compound, it is not required to practice this invention. The sulfur is preferably dispersed in the binder in an amount of from 10 to 100 parts based on the weight of the binder:

The amount of sulfur needed to facilitate core removal and/or shakeout is from 1 to 200 weight percent based on the weight of the organic binder, preferably from 10 to 100 weight percent; or from 0.1 to 2.0 weight percent based on the weight of the foundry aggregate, preferably from 0.3 to 1.0 weight percent.

5 As was mentioned previously, curing the foundry shape preferably takes place by the cold-box process. The cold-box process involves blowing or ramming the foundry mix into a pattern where it is shaped, and then curing the foundry shape with a vaporous or gaseous catalyst. Various vapor or vapor/gas mixtures or gases such as tertiary amines, carbon dioxide, methyl formate, and sulfur dioxide can be used
10 depending on the chemical binder chosen. Those skilled in the art will know which gaseous curing agent is appropriate for the binder used. For instance, epoxy-acrylic binders cured with sulfur dioxide in the presence of an oxidizing agent are described in U.S. Patent 4,526,219, which is hereby incorporated into this disclosure by reference. Alkaline phenolic resole resins cured with carbon dioxide are described in U.S. Patent
15 4,985,489, which is hereby incorporated into this disclosure by reference. Alkaline phenolic resole resins cured with methyl esters are described in U.S. Patent 4,468,359, which is hereby incorporated into this disclosure by reference.

As was mentioned previously, the preferred cold-box binder is an ISOCURE® phenolic urethane binder cured by passing a tertiary amine gas, such a triethylamine,
20 through the molded foundry shape in the manner as described in U.S. Patents 3,409,579 and 3,485,497, which are hereby incorporated into this disclosure by reference. These binders are based on a two-part system, one part being a phenolic resin component and the other part being a polyisocyanate component. Typical gassing times are from 0.5 to 3.0 seconds, preferably from 0.5 to 2.0 seconds. Purge times are from 1.0 to 60 seconds,
25 preferably from 1.0 to 10 seconds.

The phenolic resole resin used in the phenolic resin component is preferably prepared by reacting an excess of an aldehyde with a phenol in the presence of either an alkaline catalyst or a metal catalyst. The preferred phenolic resins used in the subject binder compositions are well known in the art, and are specifically described in U.S.
30 Patent 3,485,797 which is hereby incorporated by reference. These resins, known as

benzylic ether phenolic resole resins are the reaction products of an aldehyde with a phenol. They contain a preponderance of bridges joining the phenolic nuclei of the polymer, which are ortho-ortho benzylic ether bridges. They are prepared by reacting an aldehyde and a phenol in a mole ratio of aldehyde to phenol of at least 1:1 in the presence of a metal ion catalyst, preferably a divalent metal ion such as zinc, lead, manganese, copper, tin, magnesium, cobalt, calcium, and barium.

The phenols use to prepare the phenolic resole resins include any one or more of the phenols which have heretofore been employed in the formation of phenolic resins and which are not substituted at either the two ortho-positions or at one ortho-position and the para-position such as unsubstituted positions being necessary for the polymerization reaction. The aldehyde used to react with the phenol has the formula $RCHO$ wherein R is a hydrogen or hydrocarbon radical of 1 to 8 carbon atoms. The most preferred aldehyde is formaldehyde.

Organic polyisocyanates used in the organic polyisocyanate component are liquid polyisocyanates having a functionality of two or more, preferably 2 to 5. They may be aliphatic, cycloaliphatic, aromatic, or a hybrid polyisocyanate. Mixtures of such polyisocyanates may be used. The polyisocyanates should have a viscosity of about 100 to about 1,000, preferably about 200 to about 600.

Solvents are typically used in the organic polyisocyanate component and/or phenolic resin component. If solvents are used in either, those skilled in the art will know how to select them. Typical organic solvents include aromatic solvents, esters, ethers, or possibly mixtures of these solvents. In general, the solvent concentration in the polyisocyanate and/or phenolic resin component is up to 80% by weight of the polyisocyanate or phenolic resin, typically in the range of 20% to 80%.

The phenolic resin and polyisocyanate are used in sufficient concentrations to cure in the presence of the volatile amine curing catalyst. In general the isocyanate ratio of the polyisocyanate to the hydroxyl of the phenolic resin component (NCO/OH ratio), is from 1.25:1.0 to 0.60:1.0, preferably about 0.9:1.0 to 1.1:1.0, and most preferably about 1.0:1.0.

Various types of aggregate and amounts of binder are used to prepare foundry mixes by methods well known in the art. The preferred aggregate employed for preparing

foundry mixes is sand wherein at least about 70 weight percent, and preferably at least about 85 weight percent, of the sand is silica. Other suitable aggregate materials for ordinary foundry shapes include zircon, olivine, aluminosilicate, chromite sand, and the like.

5 The amount of binder needed is an amount that is effective in producing a foundry shape that can be handled or is self-supporting after curing. In ordinary sand type foundry applications, the amount of binder is generally no greater than about 10% by weight and frequently within the range of about 0.5% to about 7% by weight based upon the weight of the aggregate. Most often, the binder content for ordinary sand foundry
10 shapes ranges from about 0.6% to about 5% by weight based upon the weight of the aggregate in ordinary sand-type foundry shapes.

Optional ingredients for the binder include release agents, benchlife extenders, and adhesion promoters to improve humidity resistance, e.g. silanes as described in U.S. Patent 4,540,724 which is hereby incorporated by reference.

15

A description of the components used in the examples follows:

20	AROMATIC HYDROCARBON	=	aromatic solvent having a boiling point between about 175°C and 200°C.
	BUTYL TUADS	=	tetrabutyl thiuram disulfide, sold by R. T. Vanderbilt Co.
25	DISPERSANT	=	DISPERBYK 161, a product of BYK Chemie USA.
	DRYING OIL	=	a polylinseed oil.
	ESTER SOLVENT	=	ester solvent having a boiling point of 200 to 225° C.
30	FATTY ACID	=	a tall oil having an acid no. of 170 – 180.

MDI = a polymethylene polyphenyl polyisocyanate having a functionality of 2.5 to 2.8.

5 PHENOLIC RESIN = benzylic ether phenolic resole resin having a GPC weight average molecular weight of from about 800 to 1200 prepared by reacting phenol and formaldehyde along the lines of the process described in U.S. Patent 3,485,797.

10 S = elemental sulfur.

SILANE = ureidopropyl trimethoxysilane.

15 **EXAMPLES**

The examples will illustrate specific embodiments of the invention. These examples along with the written description will enable one skilled in the art to practice the invention. It is contemplated that many other embodiments of the invention will be operable besides these specifically disclosed.

20 The foundry binders are used to make foundry cores by the cold-box process using a tertiary amine catalyst (triethyl amine) to cure a phenolic urethane binder. All parts are by weight and all temperatures are in °C unless otherwise specified.

In Example 1, the foundry mix was prepared by first mixing elemental sulfur with Wedron 540 silica sand. Then the phenolic resin component was added and
25 mixed, followed by the polyisocyanate component. In Examples 2-4, binder Parts I and II, were mixed with the sand, and then the elemental sulfur was added to this mixture. In Examples 5, the elemental sulfur was dispersed in the phenolic resin component of the binder. Then this dispersion and the polyisocyanate component of the binder were added to and mixed with the sand.

The amounts of the various components are specified in the tables, and are in weight percent based upon the weight of the binder (bob), or in weight percent based upon the sand mixture (bos).

5 The resulting foundry mixes were shaped by blowing the foundry mix into a pattern corebox to make internal test cores that were used in casting an aluminum part. The shaped mix in the corebox was contacted with triethyl amine (TEA) at 20 psi for 1 second, followed by a 6 second nitrogen purge at 40 psi., thereby forming AFS tensile strength test cores in the shape of a dog bones. The temperature of the constant temperature room (CT) was 25°C and the relative humidity was 50%. Dog bones and
10 shakeout cores were stored in the CT room prior to testing. Dog bones (at 24 Hrs.) were also wrapped in aluminum foil and baked in a forced air oven at 750° C for 10 minutes and cooled to room temperature prior to testing.

The test cores produced were solid and shaped like a trapezoid and had a height of 1.5". There are two 5" converging sides to the trapezoid. The converging sides of
15 the trapezoid create two end "faces", one having a length of 1.50", and the other having a length of 3.75". The trapezoid test cores had three tubular stems, one on the 1.5" face and two on the 3.75" face. The stems in the trapezoid test cores were designed so that holes result in the aluminum casting made from the trapezoid test core. The hole-generating stems were 0.75" in diameter.

20 The test cores were used as internal cores to make an aluminum casting. A test core was placed in the bottom half of a sand mold designed for placement of the test core. Then the top half of the mold, which contained a sprue through which metal could be poured, was inserted on top of the bottom half.

Molten Aluminum 319 having a temperature of 730° C was poured into the
25 casting assembly and then allowed to cool. The resulting aluminum casting was a hollow trapezoid having a thickness of 0.25". There is one hole at the center of the 1.5" end face of the trapezoid and two holes on the 3.75" end face that are about 1.5" apart and each about 0.75" from the end.

Prior to testing, the cores were aged overnight in a constant temperature room at 25°C and the relative humidity of 50%. Core testing was conducted in a Lindberg box furnace with 4.5 cubic foot chamber volume. The temperature was 500° C.

The top of the trapezoid casting had a block of metal protruding from it that is used to attach the aluminum casting to the Herschal hammer during the shakeout test. For the external core removal testing, the two stems on the 3.75" face were removed and the trapezoid cores were placed up right on the 3.75" face. The shakeout tests were conducted at room temperature (cold) by attaching the aluminum casting to a 40 psi mechanical Herschal hammer to the protrusion on the trapezoid test casting. The Herschal hammer applied pressure on the casting at 15 second intervals until the internal core was removed from the aluminum casting through the holes in the test core. The amount of sand exiting the casting from the hole on the 1.5 inch face of the trapezoid casting was measured every 15 seconds.

EXAMPLES 1-4 (SULFUR IS ADDED TO AGGREGATE)

Binder formulation A, which is shown in Table I, was used in Examples 1-4. In these examples, the elemental sulfur was added to the aggregate.

TABLE I
BINDER FORMULATION CONTROL

PART I PHENOLIC RESIN COMPONENT (pbw)		PART II POLYISOCYANATE COMPONENT (pbw)	
RESIN	53.0	MDI	71.0
ESTER SOLVENT	16.7	AROMATIC SOLVENT	25.0
AROMATIC SOLVENT	29.3	DRYING OIL	4.0
FATTY ACID	1.0		

TABLE II
TENSILE STRENGTHS (PSI) OF TEST CORES PREPARED WITH AND WITHOUT SULFUR

Example	Binder Formulation (bos)		S (bos)	Average Tensile Strength (psi)			
	Part I	Part II		30 sec.	1 Hr.	24 Hr.	750° C (10 mins)
CONTROL	0.66	0.54	0.0	116	146	98	58
1	0.66	0.54	0.6	109	111	92	2

TABLE III
COLD SHAKEOUT COMPARISON WITH AND WITHOUT SULFUR

5

Shakeout Time (seconds)	Weight % Core Shakeout	
	A	1
Binder		
S (wt% bos)	0.0	0.6
15 sec.	44	100
30 sec.	75	
45 sec.	92	
60 sec.	99	
75 sec.	100	

Table III shows the effect of adding sulfur to the binder formulation. All of the sand of the internal core shook out in 15 seconds for the internal test core made with the binder containing sulfur (Example 1). On the other hand, it took the sand 75 seconds to shake out for the internal test core made with the binder which did not contain sulfur (CONTROL).

Binder formulation CONTROL again was used with varying amounts of elemental sulfur in Examples 2-4. The amount of sulfur used in the formulations is shown in Table IV. The same amount of binder (bos) was used as shown in Table II. Shakeout tests were again run. The shakeout results are shown in Table V.

TABLE IV
COLD SHAKEOUT COMPARISON WITH AND WITHOUT SULFUR

Shakeout Time (seconds)	Weight % Core Shakeout			
Example	CONTROL	2	3	4
S (wt %)	0.0	0.1	1.0	2.0
15 sec.	25	56	100	34
30 sec.	52	91		93
45 sec.	57	100		96
60 sec.	76			100
75 sec.	84			
90 sec.	89			
105 sec.	95			
120 sec.	96			

5

Table IV confirms the effect of adding sulfur to the binder formulation at different amounts. Internal test cores made with the binders containing the sulfur shook out completely in 60 seconds or less. The data also indicates there is an optimum amount of sulfur, about 1.0 part by weight bos to obtain the best shake out properties.

10

Example 5 shows a binder formulation where the sulfur is added to the binder rather than the aggregate. In this example, a sulfur dispersion was first prepared by mixing elemental sulfur, the resin, and ester solvent in the amount shown in Table V. The resulting dispersion was then mixed with the phenolic resin components of the binder in the amount indicated in Table VI.

**TABLE V
DISPERSED SULFUR**

COMPONENT	PBW
RESIN	160.0
ESTER SOLVENT	40.0
DISPERSANT	0.5
SULFUR	100.0

- 5 Table VI shows the binder formulation that was used in Example 5. The amount of Part I used in Example 5 is 133 pbw, greater by about 33% pbw than in the previous examples, but the ratio of hydroxyl groups in the phenolic resin component to isocyanato groups in the polyisocyanate component is the same as in the previous examples. The increased weight is attributable to the addition of the elemental sulfur in
- 10 the Part I.

**TABLE VI
BINDER FORMULATION CONTAINING DISPERSED SULFUR**

PART I PHENOLIC RESIN COMPONENT (pbw)		PART II POLYISOCYANATE COMPONENT (pbw)	
DISPERSED SULFUR	100.0	MDI	71.0
ESTER SOLVENT	3.8	AROMATIC SOLVENT	25.0
AROMATIC SOLVENT	28.3	DRYING OIL	4.0
FATTY ACID	1.0		

- 15 Table VIII shows shake out test data for the binder formulation set forth in Table VI.

TABLE VII
SHAKEOUT RESULTS USING BINDER FORMULATION
CONTAINING DISPERSED SULFUR

Shakeout Time (seconds)	Weight % Core Shakeout	
Example	CONTROL	5
S (wt %)	0.0	0.3
15 sec.	24	79
30 sec.	40	91
45 sec.	45	95
60 sec.	53	100
75 sec.	66	
90 sec.	80	
105 sec.	88	
120 sec.	91	

5 SS

Example 5 shows that a binder formulation, where the sulfur is added to the binder rather than the aggregate, also reduces the time for core removal. The test indicates that shakeout for the internal core made with the binder containing sulfur took less than one half the time to shakeout from the aluminum casting.

10

Examples 6-7
(Use of butyl tuads as the divalent sulfur compound)

Example 1 was repeated, except as otherwise indicated. The Control binder is described in Table VIII and the binders containing BUTYL TUADS are described in

15 Table IX.

TABLE VIII
(Control Binder)

PART I PHENOLIC RESIN COMPONENT (pbw)		PART II POLYISOCYANATE COMPONENT (pbw)	
RESIN	53.0	MDI	72.0
ESTER SOLVENT	17.0	AROMATIC SOLVENT	13.0
AROMATIC SOLVENT	28.0	KEROSENE	10.0
FATTY ACID	1.0	DRYING OIL	4.0
SILANE	1.0	BPOD	1.0

20

TABLE IX
(Binders containing butyl tuads, phenolic resin component)

PART I (Example 6) PHENOLIC RESIN COMPONENT WITH 5 WT% BUTYL TUADS		PART I (Example 7) PHENOLIC RESIN COMPONENT WITH 10 WT% BUTYL TUADS	
RESIN	53.0	MDI	72.0
ESTER SOLVENT	17.0	ESTER SOLVENT	17.0
AROMATIC SOLVENT	23.0	AROMATIC SOLVENT	18.0
FATTY ACID	1.0	FATTY ACID	1.0
SILANE	1.0	SILANE	1.0
BUTYL TUADS	5.0	BUTYL TUADS	10.0

5

The Part II for the binder was the same as that used in the Control binder described in Table VIII. The Part I and Part II were each mixed on Wedron 540 silica sand in a weight ratio of 55 Part I to 45 Part II at 1.0 wt % BOS (binder on sand) and test cores were made according to the procedure described in Example 1. The tensile strengths of the test cores were tested as set forth in Example 1. The test results are set forth in Table X.

10

Table X
(Zero bench tensile strengths [psi])

	Binder		
	Control	Example 6	Example 7
Dwell Time	Tensile Development (psi)		
30 seconds	97	102	113
	98	87	113
	109	104	114
1 hour	148	140	167
	161	150	165
	160	151	164
24 hours	167	116	159
	163	130	149
	160	136	141

15

Using the binders of Examples 6-7, eight trapezoid test cores were also prepared with Wedron 540 silica sand at 1.0 wt % BOS, but these trapezoid test cores were not cast and shaken out. Instead, the trapezoid cores were baked, side-by-side, in a Lindberg furnace at 500° C with 4.5 cubic foot chamber volume to test the collapsibility, i.e. the

time it took the core collapse when subjected to these oven temperatures. The core positions inside the oven were rotated side to side and front to back eight times. The times for core collapse were recorded. Prior to testing, the cores were aged overnight in a constant temperature room at 25°C and the relative humidity of 50%.

5 The test cores were solid and shaped like a trapezoid and had a height of 1.5". There are two 5" converging sides to the trapezoid. The converging sides of the trapezoid create two end "faces", one having a length of 1.5", and the other having a length of 3.75". The trapezoid test cores had three tubular stems, one on the 1.5" face and two on the 3.75" face. The hole-generating stems were 0.75" in diameter. For the
10 external core removal testing, the two stems on the 3.75" face were removed and the trapezoid cores were placed up right on the 3.75" face.

The results of these tests are set forth in Table XI.

Table XI
Core Collapse Times at 500° C

	Binder	
	Control	Example 7
Trial #	Time to Core Collapse (min.)	
1	70	50
2	75	51
3	58	52
4	55	50
5	68	50
6	61	52
7	64	48
8	57	50

The data in Table X indicate that cores made from the binder containing BUTYL TUADS in the phenolic resin component have similar core strength to the cores made with the Control binder that does not contain BUTYL TUADS. However, the data in
20 Table XI indicate that the time to collapse the core was consistently lower for cores made with the binder containing the BUTYL TUADS in the phenolic resin component of the binder. Accelerated external core reduces the time and energy required for core

removal. It is surprising that this can be achieved without detrimentally affecting the tensile development of the cores.

- It was also noted the cores made from the binders containing the BUTYL TUADS in the phenolic resin component bakes out to it's original color (white)
- 5 faster than the cores made with the Control binder. This indicates the thermal sand reclamation can be accelerated by incorporating BUTYL TUADS into the binder formulation.